

## PRESSURE-TUNED SOLID CATALYZED HETEROGENEOUS CHEMICAL REACTIONS

### BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

The present invention is broadly concerned with improved methods of conducting solid acid-catalyzed, near- or supercritical heterogeneous chemical reactions such as alkylation reactions in order to improve the efficiency thereof and the tendency for the reactions to be prematurely terminated owing to coke laydown on the catalyst. More particularly, the invention is concerned with such methods wherein reaction product selectivity is enhanced by pressure-tuning the reaction together with use of particular types of solid acid catalysts having relatively narrow surface area and pore size characteristics. The invention also provides a way of substantially continuously maintaining a chemical reaction by appropriately timed catalyst regeneration cycles during the course of the reaction.

#### 2. Description of the Prior Art

Conventional isoparaffin/olefin alkylation processes, practiced since the 1930's, convert light refinery gases to high octane number gasoline range hydrocarbons (e.g. trimethylpentane) using liquid sulfuric or hydrofluoric acid catalysts. These processes typically convert refinery gasses such as  $C_4$ - $C_5$  isoparaffins into more valuable branched chain gasoline-range  $C_7$ - $C_9$  alkylate compounds. Particularly valuable alkylates are trimethylpentanes (TMPs) and 2,2-dimethylbutane (neohexane) which are used as high-octane blending components for aviation and civilian gasolines. It is estimated that about 13% of the U.S. gasoline pool is made up of alkylates.

However, economic and environmental concerns associated with liquid acid catalyst handling, regeneration, and disposal, have spurred the search for an alternative process. Since the early 1970's, the use of solid acid catalysts as a replacement has been investigated (Corma, et al., *Catal. Rev.-Sci. Eng.*, **35** (1993) 483), but in many instances the results have been disappointing. The reason is that solid acid catalysts tend to deactivate rapidly with time due to buildup of heavy hydrocarbons on the catalyst surface. The deactivating pathway is believed to

suppress the hydride transfer mechanism, which is dependant on the acid site density (Pater, J., et al. *Ind. Eng. Chem. Res.* **38** (1999) 3822). Among the most common solid acids to be investigated are zeolites, sulfated zirconia, and aluminum chloride. (Corma, et al., *Catal. Rev.-Sci. Eng.*, **35** (1993) 483; Rao, P., et al., *Prep.-Div. Pet. Chem. ACS*, **41** (1996) 685; and  
5 Weitkamp, J. and Traa, Y. *Catal. Today*, **49** (1999) 93).

U.S. Patent No. 5,907,075 represents a significant advance in the art and describes improved solid acid catalyst supercritical alkylation processes which ameliorate the catalyst coking problem. The '075 patent teaches that use of a co-solvent or diluent such as CO<sub>2</sub> together with supercritical reaction conditions have the effect of lessening the coke laydown difficulty.  
10 However, after a certain period of reaction time, the catalyst will nevertheless become deactivated because of coke buildup, and a "breakthrough" will occur, meaning that the production of desired reaction product will decline usually in a precipitous fashion.

The liquid-like densities yet significantly better-than-liquid diffusivities of supercritical (*sc*) reaction media have been shown to be more desirable than either liquid or gas phases to  
15 mitigate catalyst deactivation by coking (Subramaniam, B., *Appl. Catal.* **212** (2001) 199). Gas phase isobutane/butene alkylation is not practical because of the low volatility of the primary products (C<sub>8</sub>'s), which undergo subsequent reaction such as oligomerization on the catalyst resulting in rapid catalyst deactivation. Operation in a liquid phase provides the maximum solubility for removing adsorbed heavy hydrocarbons. However, the pore diffusion rate in a  
20 liquid is much lower than that in a gas phase. This increases the likelihood of readsorption and further reaction of the solvated molecules in the pore.

It has been shown in the literature that isobutane ( $P_c = 36.5$  bar,  $T_c = 408$  K)/butene ( $P_c = 40.2$  bar,  $T_c = 420$  K) alkylation on solid acid catalysts at supercritical temperatures suffers from increased butene oligomerization and cracking reactions at these temperatures, increasing the  
25 catalyst deactivation potential (Fan, L., et al. *Ind. Eng. Chem. Res.*, **36** (1997) 1458; Funamoto, G., et al. *Res. Chem. Intermed.*, **24** (1998) 449; and Gayraud, P., et al. *Catal. Today*, **63** (2000) 223). Lower temperatures tend to favor the alkylation reaction. Supercritical operation at 95°C can be facilitated by diluting the isoparaffin/olefin feed with suitable amounts of a low  $T_c$  inert solvent such as CO<sub>2</sub> ( $P_c = 73.8$  bar,  $T_c = 304$  K), and has been shown to give rise to steady  
30 alkylation activity on USY and beta zeolites (Clark, M., et al., *Ind. Eng. Chem. Res.*, **37** (1998)

1243). However, the alkylate yields are very low (< 10%) on these catalysts, attributed to severe pore diffusion limitations on these catalysts.

Nafion<sup>®</sup> is a perfluorinated polymer with sulfonic acid groups grafted to side chains, yielding acidity similar to that of sulfuric acid (Fărcașiu, D. et al. *J. Am. Chem. Soc.*, **119** (1997) 11826). Nafion<sup>®</sup> has not been extensively studied as a catalyst for isoparaffin alkylation, although it has shown good activity for a number of acid catalyzed reactions (Olah G., et al. *Synthesis* (1978) 672; Chaudhuri, B., et al., *Ind. Eng. Chem. Res.*, **30** (1991) 227; Yamato, T., et al., *J. Org. Chem.*, **56** (1991) 2089; and Sun, Q., et al. *Ind. Eng. Chem. Res.*, **36** (1997) 5541). Nafion<sup>®</sup> is available in both unsupported and supported forms. In the supported form, the polymer is impregnated on high surface area silica supports, which has been shown to improve accessibility to acid sites (Harmer, M., et al. *Chem. Comm.*, (1997) 1803; and Sun, Q., et al. *Ind. Eng. Chem. Res.*, **36** (1997) 5541).

Rørvik, et al. studied unsupported Nafion<sup>®</sup> for isobutane/1-butene alkylation in a stirred liquid phase batch reactor (Rørvik, T., et al. *Catal. Lett.*, **33** (1995) 127). The production of trimethylpentanes (the most desirable alkylate product) was shown to cease within 30 minutes of operation. More recently, silica-supported Nafion<sup>®</sup> was used to catalyze the same reaction (Botella, P., et al. *J. Catal.*, **185** (1999) 371). Once again, rapid deactivation with respect to trimethylpentane formation was observed. It was hypothesized that the strongest acid sites—the most active for alkylation—are also the first to be poisoned.

## SUMMARY OF THE INVENTION

The present invention overcomes the problems outlined above and provides improved methods for conducting acid-catalyzed heterogeneous chemical reactions using a reactant mixture comprising one or more heterogeneous reactant(s) (e.g., alkylation, acylation, isomerization, aromatic disproportionation, alcohol synthesis, and Fischer-Tropsch reactions) under near- or supercritical conditions, in order to avoid, or at least substantially control, problems heretofore encountered in such reactions owing to coke laydown. Broadly speaking, in one aspect of the invention, it has been found that use of particular types of macroporous solid catalysts significantly delays the onset of catalyst deactivation owing to coke laydown under supercritical reaction conditions. In another aspect, it has been discovered that heterogeneous reactions of this type may be pressure-tuned to maximize selectivity of desired end products, while also

permitting regeneration of the solid catalyst prior to significant catalyst deactivation; this permits use of a dual reactor system wherein the respective reactors may be used in an alternate fashion, cycling between reaction duty and catalyst regeneration.

In more detail, in preferred forms of the invention, the catalyst used in heterogeneous  
5 near- or supercritical chemical reactions should have a BET surface area of from about 50-400  $\text{m}^2/\text{g}$ , and more preferably from about 10-300  $\text{m}^2/\text{g}$ , and most preferably about 200  $\text{m}^2/\text{g}$ . The catalyst should also have an average pore size on the order of from about 70-150 Å, more preferably from about 80-120 Å, and most preferably about 100 Å. Although a number of solid catalysts can be used to good effect, supported perfluorinated polymer catalysts having sulfonic  
10 acid groups coupled thereto are preferred, such as the known Nafion® catalysts. This preferred catalyst has the following characteristics:  $\text{SiO}_2$  support - 87% wt%  $\text{SiO}_2$  (CAS 112945-52-5), 13% tetrafluoroethylene-perfluoro-3,6-dioxane-4-methyl-7-octenesulfonic acid copolymer (CAS 31175-20-9), BET surface area  $\sim 200 \text{ m}^2/\text{g}$ , acid capacity 0.14 meqH/G; Nafion® - a solid superacid catalyst ion exchange polymer (exhibiting an acid strength comparable to that of  
15  $\text{H}_2\text{SO}_4$ ) including a perfluorocarbon backbone with sulfonic acid side groups. Other suitable catalyst resins would include Amberlyst® (sulfonated polystyrene divinyl benzene resin), Ionac® (sulfonated polystyrene divinyl benzene resin) and Deloxan® (sulfonated polysiloxane resin), where such resins would be used with a solid support such as  $\text{SiO}_2$ .

Reaction conditions should typically be in the neighborhood of from about 0.9-1.3  $T_c$  of  
20 the reactant mixture (i.e., the reactant(s) fed to the reactor), and more preferably from about 1.01-1.2  $T_c$ . Similarly, pressure conditions are advantageously maintained at a level of from about 0.9-2.5  $P_c$  of the reactant mixture, more preferably from about 1.01-1.2  $P_c$  thereof.

Where continuous heterogeneous reactions are contemplated which include a co-solvent or diluent, improvements are obtained by periodic catalyst regeneration cycles during the course  
25 of a substantially steady state reaction. Thus, the solid acid catalysts may be regenerated by terminating introduction of at least one of the reactant(s) to the reactor prior to a time when the solid catalyst is significantly deactivated owing to coke laydown. Thereupon, the pressure within the reactor is elevated and/or the temperature therein is lowered to remove at least a portion of any coke on the catalyst. When this is accomplished, the chemical reaction may be resumed by  
30 reestablishing substantially steady state conditions within the reactor and again commencing full introduction of reactant(s) into the reactor.

In more detail, it is desired that the catalyst regeneration be carried out before the rate of production of a desired reaction product falls by a factor of 20% (more preferably 35%), as compared with the steady state reaction product production rate before the catalyst regeneration step. In practice, the appropriate time to begin the catalyst regeneration can be readily  
5 determined by ascertaining when the "breakthrough" for the reaction occurs, that is when the characteristic rapid decline in production of the desired reaction product(s) is observed. It has been found the continuity of heterogeneous reactions may be maintained almost indefinitely by proper cycling of a reactor between reaction and catalyst regeneration stages. Generally speaking, the higher pressure catalyst regeneration step is carried out at pressures which are  
10 elevated by at least about 40%, as compared with the pressure within the reactor during the normal chemical reaction. In many instances, the higher regeneration pressures are obtained by introduction of additional high pressure CO<sub>2</sub> or other co-solvent or diluent; CO<sub>2</sub> may be used alone or mixed with other solvents such as ethane or isobutane to obtain a better removal of coke from the catalyst (in this context, "coke" refers to extractable carbonaceous deposits left on the  
15 surface of the catalyst). Where the temperature is lowered during catalyst regeneration, care should be taken to insure that the reactor temperature remains above the T<sub>c</sub> of the co-solvent or diluent. It will also be appreciated that in some instances the coke derived from catalyst regeneration may itself be a valuable or desired product, and that the coke may be conventionally recovered in such cases.

20 On a fundamental level, the invention utilizes the pressure-tunable properties of near- or supercritical reaction mixtures for the simultaneous reaction and product separation during heterogeneous catalytic reactions. The physical properties such as density, diffusivity, heat capacity, etc. of a near- or supercritical reaction mixture are very sensitive to small changes in pressure. For a reaction being conducted in a single phase, the products often have different  
25 critical properties and/or solubilities as compared with the starting reactants. As a consequence, some of the products formed in the catalyst pores may dissolve in the near- or supercritical reaction mixture, while the formation of heavier products can cause a second liquid or solid phase to form. By carefully choosing suitable operating conditions which cause selected products to be removed from the catalyst while retaining the heavier products inside the catalyst  
30 pores, certain products can be preferentially deposited in the catalyst pores, resulting in product separation. In effect, the catalyst pores act as a reservoir for selected products. At a later time

when the pores can no longer hold the heavier products without the catalyst undergoing significant deactivation, the operating conditions in the reactor are adjusted to regenerate and clean the catalyst pores so that the heavier products are dissolved and extracted out of the catalyst pores. Once the pores are clean (i.e., the catalyst is regenerated) the initial operating steady state  
5 conditions may be reestablished and the simultaneous reaction/*in situ* product separation step is repeated. These chemical reaction/catalyst regeneration cycles can be repeated continuously.

The invention finds particular utility in alkylation reactions wherein reactants include an isoparaffin, an olefin, and a molar excess of an inert co-solvent or diluent. Preferably, the isoparaffin is selected from the group consisting of C<sub>4</sub>-C<sub>10</sub> isoparaffins, and said olefin selected  
10 from the group consisting of the C<sub>2</sub>-C<sub>10</sub> olefins. Reaction conditions for the alkylation reactions typically are: pressure from about 500-3,000 psi, more preferably from about 1,000-2,500 psi; temperature from about 325-450K, more preferably from about 350-400K. The peroxide content of the reaction mixture should be no more than about 200 ppm, preferably below about 100 ppm. Furthermore, the co-solvent or diluent having a critical temperature less than the critical  
15 temperatures of each of the isoparaffin and olefin. The preferred co-solvent or diluent is selected from the group consisting of carbon dioxide, methane, ethane, hydrogen, and mixtures thereof. Finally, the reaction mixture should have a fluid density of from about 0.05-0.65 g/cc. Generally speaking, the reaction conditions useful for alkylation reactions are those set forth in U.S. Patent No. 5,907,075 incorporated by reference herein.

20 It has been found that butene conversion and production of desirable C<sub>8</sub> alkylates are significantly increased in the present invention. For example, in prior processes butene conversions of 10-15% and 5-10% yields of C<sub>8</sub> alkylates are common. However, with the present invention 75-80% butene conversions and 25-30% C<sub>8</sub> alkylate yields are readily attainable.

#### 25 BRIEF DESCRIPTION OF THE DRAWING FIGURES

FIG. 1 is a schematic representation of the reaction equipment employed in carrying out alkylation methods in accordance with the invention;

FIG. 2 is a graph illustrating butene conversion versus time in an alkylation method pursuant to the invention;

30 FIG. 3 is graph illustrating butene conversion versus pressure during an alkylation reaction, which demonstrates the pressure-tuning aspect of the present invention;

FIG. 4 is a graph illustrating butene conversion versus time using silica-supported Nafion solid catalyst in both liquid and supercritical phases;

FIG. 5 is a graph illustrating butene turnover versus time in alkylation reactions using supported and unsupported catalysts, respectively;

FIG. 6 is a graph illustrating butene conversion versus time in alkylation reactions using different reactor configurations;

FIG. 7 is a graph illustrating butene conversion,  $C_8$  selectivity and  $C_{12}$  selectivity versus time for an alkylation reaction including periodic catalyst regeneration steps;

FIG. 8 is a graph illustrating butene conversion,  $C_8$  selectivity and  $C_{12}$  selectivity versus time in an alkylation reaction, which demonstrates a significant decrease in  $C_8$  selectivity after approximately 50 hours of reaction run time;

FIG. 9 is a graph illustrating butene conversion,  $C_8$  selectivity and  $C_{12}$  selectivity versus time in a pressure-tuned alkylation reaction, demonstrating a significant shift in product selectivity owing to pressure-tuning; and

FIG. 10 is a schematic representation of a parallel alkylation reactor system permitting automated, alternate reaction and catalyst regeneration.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The following examples set forth preferred techniques for carrying out the heterogeneous, solid-catalyzed reaction methods in accordance with the invention. It is to be understood, however, that these examples are provided by way of illustration only, and nothing therein should be considered as a limitation upon the overall scope of the invention.

#### EXAMPLE 1

In this example, a series of supercritical condition alkylation reactions of butene and isoparaffin with a molar excess of carbon dioxide were carried out using a preferred catalyst in order to demonstrate temporal and selectivity profiles for the reactions.

The reactor schematic is shown in Fig. 1. Continuous stirred tank reactor (CSTR) experiments were conducted in a 50 mL Microclave from Autoclave Engineers, rated to 344 bar and 616 K. Catalyst particles were suspended in the reaction mixture by an impeller operating at 1200 RPM. Fixed-bed reactor experiments were conducted in a 1" I.D. stainless steel tubular

reactor from Autoclave Engineers, rated to 1110 bar at 700 K. The catalyst bed was supported on both ends with glass wool (Alltech) and stainless steel mesh screens, which were confirmed to be inert under reaction conditions.

The catalysts investigated were characterized before and after use. Unsupported Nafion<sup>®</sup> polymer beads and 13% Nafion<sup>®</sup> on silica (SAC-13) catalysts were furnished by DuPont and Engelhard Corp., respectively. Surface area (SA) and pore volume (PV) measurements were done using a Micromeretics Gemini instrument, employing nitrogen physisorption. The acid site concentration was measured by a NaCl ion-exchange/ NaOH titration procedure provided by Engelhard Corp. Catalysts were pretreated in-situ under flowing helium at 423 K for 5 hours. Unsupported Nafion<sup>®</sup> particles were 20~30 mesh, and could not be size reduced due to their pliable texture. Silica-supported Nafion<sup>®</sup> particles were size reduced to an average particle size less than 100  $\mu\text{m}$ .

Table 1 below sets forth estimated critical properties of the alkylation reactants and the carbon dioxide co-solvent/diluent.

Table 1

System (% <sub>a</sub> molar basis)	T <sub>c</sub> (K)	P <sub>c</sub> (bar)
<i>i</i> -C <sub>4</sub> (83), C <sub>4</sub> <sup>=</sup> (17)	408	36
CO <sub>2</sub> (70), <i>i</i> -C <sub>4</sub> (25), C <sub>4</sub> <sup>=</sup> (5)	340	74
CO <sub>2</sub> (73), <i>i</i> -C <sub>4</sub> (21), 2,2,4-TMP (5)	353	91

The isobutane and 1-butene feeds (Matheson, 99+%) were pre-mixed to a specified I/O ratio, analyzed offline, and then transferred to an ISCO LC5000 syringe pump. During experiments, the hydrocarbon feed was pretreated online with a 6 g neutral alumina (Fisher Scientific) trap to remove any organic peroxides, which are known to be prolific coke-precursors and can contribute to catalyst deactivation (Clark, M., et al., *AIChE J.*, **45** (1999) 1559). Carbon dioxide (Airgas, 99+%) was pumped using a cooled ISCO LC5000 syringe pump. The CO<sub>2</sub> stream was pretreated online with 6 g anhydrous sodium sulfate (Fisher) to remove moisture, and 6 g neutral alumina.



Reaction pressure was maintained with a dome-loaded back-pressure regulator (Circle Seal Controls). All heated zones were controlled and monitored with a Camile 2500 data acquisition system (Camile Products). Products were analyzed online by gas chromatography with an HP 5890 II GC, equipped with an FID, and a DB-Petro 100 m column (J&W Scientific),  
5 operated at 35° C for 30 min, ramped at 1.5°/min to 100° C, 5°/min to 250° C for 15 min. An alkylate reference standard (Supelco) allowed identification of the trimethylpentanes (TMP) and dimethylhexanes (DMH). The combined mass of TMP and DMH is referred to hereafter as the "alkylate product". As discussed elsewhere (Clark, M., et al., *Ind. Eng. Chem. Res.*, **37** (1998) 1243), propane, an impurity in the isobutane feed, was used as an internal standard for butene  
10 conversion calculations. Since isomerization from 1-butene to 2-butene isomers is rapid over acidic catalysts, reported conversion is for all butene isomers to C<sub>5</sub> and higher products. Isobutylene formation was not observed under any conditions.

Reactor startup consisted of setting the final system temperature and pressure with CO<sub>2</sub> (or pure isobutane when CO<sub>2</sub> was not used) and starting the olefin feed pump (defined as zero  
15 time). Prior to shutdown, the reactor was flushed with CO<sub>2</sub> at reaction temperature and pressure until no hydrocarbons were observed in the effluent, following which the reactor was cooled and depressurized.

Temporal conversion and selectivity profiles obtained over a silica-supported Nafion<sup>®</sup> catalyst in a stirred reactor operated at supercritical conditions are shown in Fig. 2. The  
20 experiment was carried out at 80 bar, 368 K, and 0.05 h<sup>-1</sup> OWHSV, using a 5:1 isoparaffin/olefin (I/O) ratio and 2.4 fold molar excess of CO<sub>2</sub> [(CO<sub>2</sub>+I)/O=19]. At these conditions, a steady butene conversion (80%) and product selectivity were demonstrated for 48 hours on stream. The alkylate selectivity (TMP+DMH) and overall C<sub>8</sub> selectivity are constant at 27% and 75% respectively. Clearly, operation in the near-supercritical region facilitates superior alkylate  
25 production over prior results using Nafion<sup>®</sup> catalysts in the liquid phase (Rørvik, T., et al. *Catal. Lett.*, **33** (1995) 127; Botella, P., et al. *J. Catal.*, **185** (1999) 371). Table 2 shows the steady state product distribution. While the C<sub>8</sub> paraffins (28 wt% of all products) are the most desired products, the large fraction of C<sub>8</sub> olefin (46%) is also a valuable product because of its high octane number.

Table 2. Typical Product Distribution on SAC-13 at Steady-state Conditions.

368 K, 80 Bar, I/O=5, 0.05 h<sup>-1</sup>

Product	% (mass)
C <sub>5</sub> -C <sub>7</sub>	15
Total C <sub>8</sub> 's	74
{ TMP's	11
{ 2,2,4-	5
{ 2,2,3-	4
{ 2,3,4-	2
DMH's	17
C <sub>8</sub> olefin	46
C <sub>9</sub> +	11

## EXAMPLE 2

In order to investigate the effect of pressure-tuning on catalyst activity and product selectivity, a series of separate alkylation experiments was carried out at supercritical pressures between 80 and 167 bar. All other conditions were identical: 368 K, 0.05 h<sup>-1</sup>, I/O=5, 2.4 fold excess CO<sub>2</sub>, 1200 rpm. Each run was performed for at least 24 hours, and the steady-state averages (between 10 hours and end-of-run) for conversion and selectivity are shown in Fig. 3. The steady butene conversion (~80%) is relatively independent of pressure. At the highest supercritical pressure (167 bar), the alkylate selectivity is lowest at 7%, and the overall C<sub>8</sub> selectivity is approximately 30%. As the pressure is decreased towards the critical pressure, the observed alkylate selectivity increases nearly fourfold. The results are interpreted as follows: at near-supercritical pressures, heavier compounds (C<sub>12</sub>+) are preferentially retained in the macropores. This *in situ* separation enhances the C<sub>8</sub> selectivity observed in the effluent. At higher pressures, the C<sub>12</sub> compounds are solubilized more effectively by the reaction mixture and therefore less are retained in the pores, adversely affecting C<sub>8</sub> selectivity in the effluent. Below 80 bar (i.e. sub-critical pressures), the alkylate production did not reach a steady value, but gradually decreased with time. The deactivation is attributed to substantial product condensation in the catalyst pores at subcritical pressures.

The characteristics of the fresh catalysts are shown in Table 3. The 13% Nafion<sup>®</sup>/silica-supported SAC-13 has the advantage of a surface area several orders of magnitude greater than the unsupported polymer, thereby better exposing the acid sites for reaction. In the presence of

compressed CO<sub>2</sub>, the polymeric form of Nafion<sup>®</sup> suffered from swelling and sticking, demonstrating another advantage to the silica-supported form. Post run surface area and pore volume measurements gave roughly 70% and 90% of fresh values respectively, and did not display a systematic trend at various conditions—even in liquid phase operation. This is in contrast to the results obtained on Y zeolite (Clark, M., et al., *Ind. Eng. Chem. Res.*, **37** (1998) 1243), which showed a greater loss in surface area for a liquid phase than for a near-critical CO<sub>2</sub> phase. The very small pore sizes in Y zeolite (~13 Å) are more susceptible to pore blocking than the silica support (~95 Å). The titration of Nafion<sup>®</sup> and SAC-13 catalysts' acid sites after use showed generally 90% of fresh values, again with no systematic trend.

Table 3. Acidity, Surface Area (SA) and Pore Volume (PV) of Fresh Catalysts

Catalyst	Acidity (meq/g)	SA (m <sup>2</sup> /g)	PV (cm <sup>3</sup> /g)
Unsupported Nafion	0.793	~0.01	n/a
SiO <sub>2</sub> supported Nafion (SAC-13)	0.015	220	0.508

Fig. 4 shows the butene conversion over the silica-supported Nafion<sup>®</sup> catalyst in both liquid and supercritical phases at 368 K, an OWHSV of 0.05 h<sup>-1</sup> and an I/O ratio of 10. The liquid phase was maintained at a pressure of 26 bar, while the supercritical phase was maintained at 95 bar, with a 2.4 fold molar excess of carbon dioxide (~70% total mole fraction CO<sub>2</sub>). In both cases, a high steady butene conversion is observed. However, the alkylate selectivity continuously declines to zero after 45 hours on stream, at which point the catalyst is only active for butene oligomerization. At the supercritical condition, the acid sites responsible for alkylation are kept active, extending the production of the desired trimethylpentanes. Similar results comparing liquid and supercritical phase runs were also seen on unsupported Nafion<sup>®</sup>.

Fig. 5 compares the activity of the silica-supported SAC-13 with unsupported Nafion<sup>®</sup> particles. Both catalysts show similar product selectivity at identical conditions. The butene turnover frequency, defined as the butene conversion rate per acid site, is enhanced fourfold when using the supported catalyst. Similar enhancements on supported Nafion<sup>®</sup> have been

reported for other reactions as well (Harmer, M., et al. *Chem. Comm.*, (1997) 1803; Sun, Q., et al. *Ind. Eng. Chem. Res.*, **36** (1997) 5541; and Pálínkó, I., et al. *App. Catal. A*, **174** (1998) 147. Since hydrated Nafion<sup>®</sup> can conduct protons, acid sites that are hidden within the polymer may not be available for reaction, but may still be measured by the aqueous titration method.

5        The effect of temperature was examined over the range of 358 K to 378 K, keeping all other conditions constant. Only mild effects in conversion and selectivity were observed, as seen in Table 4. Increasing temperatures tend to favor the oligomerization of butene and the cracking of heavy compounds, as evidenced by a declining C<sub>8</sub> selectivity. The net result is that the alkylate yield is not significantly affected over this temperature range.

10        Table 4. Temperature Effect on Butene Conversion and Alkylate Selectivity  
Over SAC-13. 80 bar, 0.05 h<sup>-1</sup>, I/O=5, 70 mole% CO<sub>2</sub>

Temp- erature (K)	Butene Conversion (%)	Alkylate/ C <sub>5</sub> + (%)	C <sub>8</sub> / C <sub>5</sub> + (%)
358	70	24	79
368	77	28	76
378	78	27	64

15        An alternate startup procedure was also tested. Since CO<sub>2</sub> at 80 bar and 95° C is less dense than the final reaction mixture, initial catalyst deactivation could possibly have occurred during this startup period. To address this possibility, instead of initially charging the reactor with only carbon dioxide, a 70/30 mixture of CO<sub>2</sub>/isobutane was added, followed by establishing the final temperature and pressure before adding the olefin. The results showed no dependence  
20        on the startup procedure.

The dimerization of butene is expected to be a second order process while alkylation would be a pseudo-first order rate process. By this rationale, a CSTR should provide enhanced alkylation activity compared to a PFR. As seen in Fig. 6, CSTR operation gives a steady alkylate

selectivity, as already described, whereas the PFR shows a different steady state with lower alkylate selectivity, favoring higher molecular weight compounds in the product.

### EXAMPLE 3

5           In this example a multiple-cycle alkylation experiment was performed, with successive alkylation and catalyst regeneration cycles.

10           10 g of silica-supported Nafion<sup>®</sup> acid catalyst (SAC-13, provided by Engelhard Corp.) was loaded into the reactor, and pretreated in dry nitrogen at 423 K and atmospheric pressure for 6 hours.

15           The reactor was a 50 mL stirred vessel (Autoclave Engineers) with an electrical heating jacket controlled by a CAMILE data acquisition and control system. The catalyst particles, between 62 and 105  $\mu\text{m}$ , were suspended in the fluid by intense stirring at 1200 RPM. The reactor was purged and pressurized with carbon dioxide at 368 K and 87 bar. The isobutane/1-butene mixture was premixed to a molar ratio of 5:1, and pumped from an ISCO syringe pump.  
20           This feed was pumped at 5.4 mL/hr through a 6 g bed of neutral alumina, to adsorb any organic peroxides (which are known to be prolific coke precursors). Carbon dioxide was pumped at 6.6 mL/hr from an ISCO syringe pump (cooled to 280 K), and was passed through a bed of 6 g alumina and 6 g sodium sulfate, to adsorb any moisture in the  $\text{CO}_2$  stream. The combined feed stream was fed to the bottom of the reactor. Pressure control in the reactor was maintained by  
25           a dome-loaded back-pressure regulator. The effluent stream was fitted with 5 mm and 0.5 mm filters to prevent particulates from entering the back-pressure regulator. The effluent was maintained at reaction temperature until after the pressure regulator to keep the mixture in a supercritical state. Past the back-pressure regulator, the atmospheric pressure gas was maintained at 473 K and is sampled in a HP 5890 II gas chromatograph equipped with a flame ionization  
30           detector and a DB Petro 100 m capillary column (J&W Scientific).

          The combined feed was passed through the reactor for 30 hours at 368 K and 87 bar. After this time, the catalyst regeneration step was started. The hydrocarbon feed was stopped, and the carbon dioxide feed was increased to 1 mL/min. The pressure was increased to 140 bar. Carbon dioxide was allowed to clean the catalyst pores for 9 hours. The pressure was returned  
35           to 87 bar and the original feed flow rates were established for the next cycle. Fig. 7 illustrates the results of this test and confirms that after each regeneration step the catalyst retained a

substantial fraction of its activity, as compared with the first reaction cycle activity (usually at least about 85%).

#### EXAMPLE 4

5 In this example, an isobutane/1-butene alkylation reaction in  $\text{CO}_2$  was carried out under supercritical conditions, using the preferred solid Nafion® catalyst. The results of this test are set forth in Fig. 8, a graph of % conversion of butene,  $\text{C}_8$  selectivity and  $\text{C}_{12-}$  selectivity over time. The reaction conditions were 368K, 78 bar, other conditions as set forth in Example 1.

10 As shown, there is a "breakthrough" of high molecular weight compounds with increasing reaction time. At the specified operating conditions, the breakthrough typically occurs at 35-50 hours reaction time. Note the dramatic drop in selectivity of the desired  $\text{C}_8$  products, and the corresponding rise in production of undesired  $\text{C}_{12-}$  compounds, while butene conversion is relatively unaffected. As discussed in Example 5, it is possible to periodically clean the pores (before  $\text{C}_8$  selectivity decline occurs) by dissolving the retained heavier compounds with high-  
15 pressure  $\text{CO}_2$ .

#### EXAMPLE 5

In this example, this effect of pressure-tuning on final productivity in an alkylation reaction was investigated.

20 The experiment was conducted as described in Example 3, with the isobutane/1-butene alkylation carried out under supercritical conditions (368K, variable pressure). The reactor pressure was maintained at 83 bar for 22 hours, and at 137 bar thereafter.

The results of this test are plotted in FIG. 9, demonstrating the dramatic shift in selectivity which occurs when the pressure is increased, causing increased solubility of higher molecular  
25 weight products. Here, the feed flow rates are unchanged- only the reactor pressure is changed at 22 hours. A mass balance indicates that at the time of the pressure change, more hydrocarbons are leaving the reactor than are being fed. This suggests the heavy products were being "stored" inside the reactor prior to the pressure change.

30 As indicated previously, the pressure-tuning aspects of the present invention permit relatively long runs while avoiding significant product selectivity degradation. Fig. 10 schematically depicts an automated apparatus to achieve this end. The apparatus 10 includes first

and second catalytic reactors 14 each having valve-controlled reactant and co-solvent or diluent inputs 16 and 18, respectively. The output lines 20, 22 from the reactors 12, 14 are also valve-controlled and pass through appropriate analyzers 24, 26 (typically gas chromatographs) designed to analyze product outputs. A process controller 28, usually in the form of a microprocessor is operably coupled with the input and output lines to the reactors 12, 14, as well as the analyzers 24, 26 as shown.

In practice, during the time that reactor 12 is being used for the desired heterogeneous reaction, the reactor 14 will be undergoing a catalyst purge/reactivation cycle. When the latter is completed, the controller 28 will then reverse the reactors, so that the catalyst within reactor 12 is treated and the desired chemical reaction is carried out in reactor 14. Generally speaking, a system of this type can readily be employed, once the breakthrough time for the reaction in question is determined, as explained in Example 4 and Fig. 8.